# The Thermal Field Dislocation Mechanics (T-FDM) model

Upadhyay, M. V., On the thermo-mechanical theory of field dislocations in transient heterogeneous temperature fields, *Journal of the Mechanics and Physics of Solids*, 105 (2020) 104150

https://doi.org/10.1016/j.jmps.2020.104150

- Development
  - The isothermal and adiabatic FDM model
  - Heat conduction
  - The new T-FDM model
- Model assumptions and impact on AM modelling



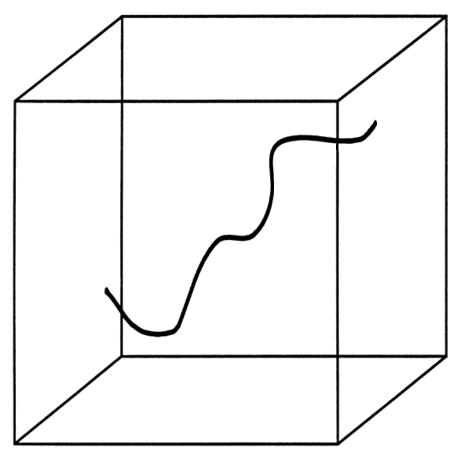
# The Thermal Field Dislocation Mechanics (T-FDM) model

Upadhyay, M. V., On the thermo-mechanical theory of field dislocations in transient heterogeneous temperature fields, *Journal of the Mechanics and Physics of Solids*, 105 (2020) 104150

### • Development

- The isothermal and adiabatic FDM model
- Heat conduction
- The new T-FDM model
- Model assumptions and impact on AM modelling





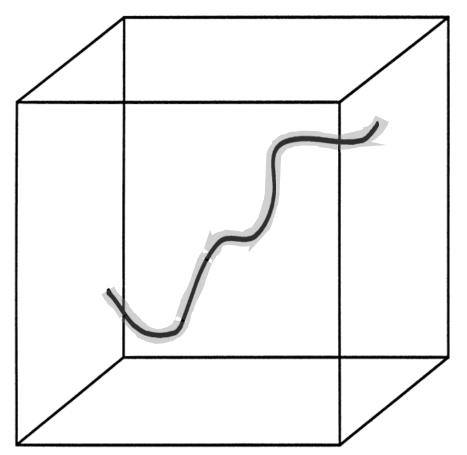
Discrete representation

#### A line (singular) defect

Michell 1899, Timpe 1905, Weingarten 1901, Volterra 1907, Love 1944, Nabarro 1967, Hirth & Lothe 1982

Adapted from Arsenlis, Parks, Acta Mat. (1999)





Discrete representation

#### A line (singular) defect

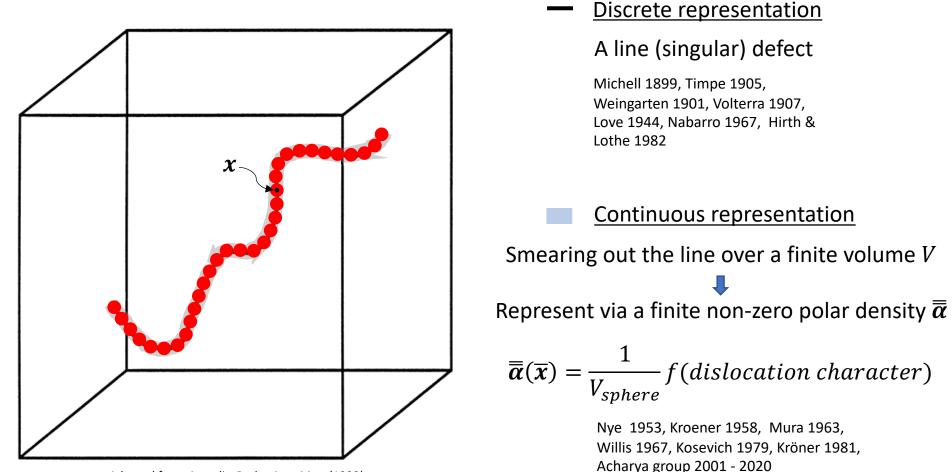
Michell 1899, Timpe 1905, Weingarten 1901, Volterra 1907, Love 1944, Nabarro 1967, Hirth & Lothe 1982

#### Continuous representation

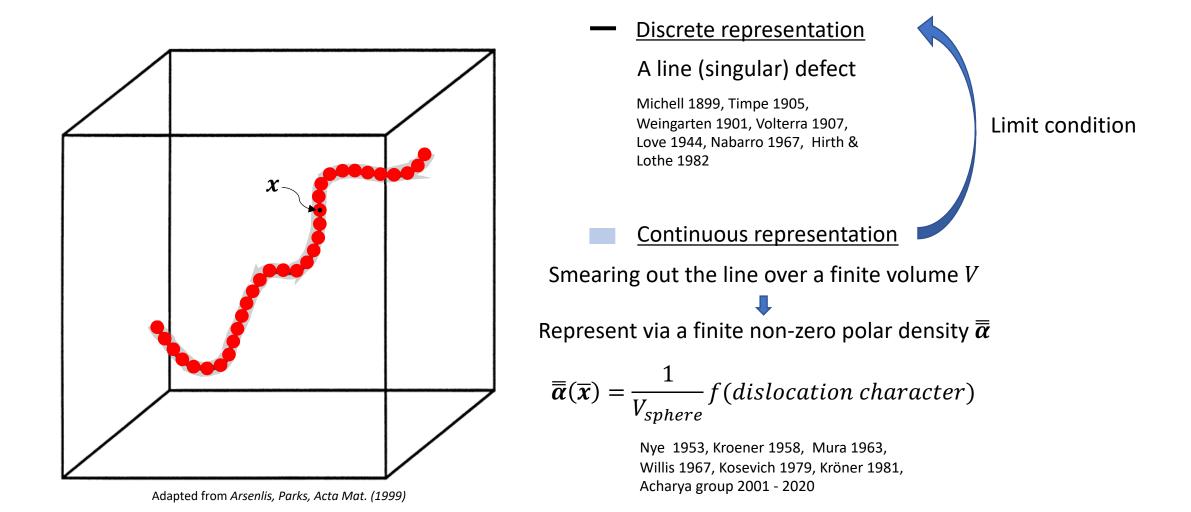
Smearing out the line over a finite volume V

Adapted from Arsenlis, Parks, Acta Mat. (1999)



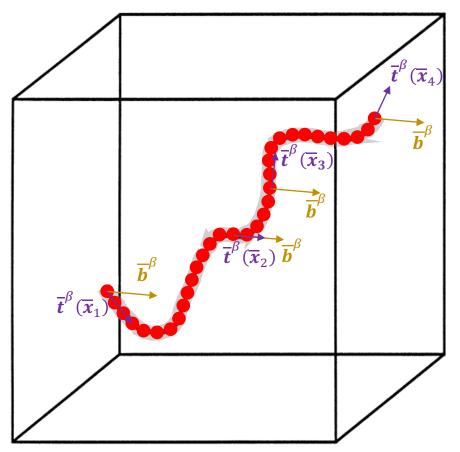


Adapted from Arsenlis, Parks, Acta Mat. (1999)





## Theory of continuously represented dislocations: characterization



<u>A single dislocation on a slip system  $\beta$ </u>

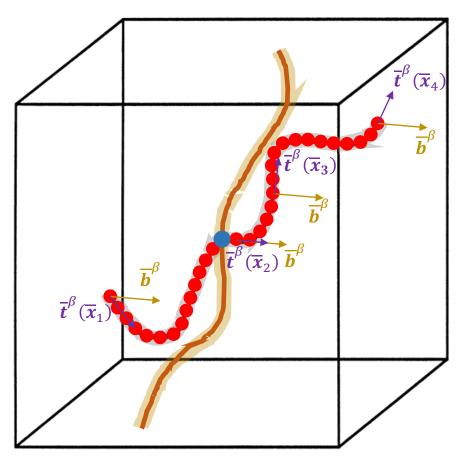
Characterized via Burgers vector  $\overline{\boldsymbol{b}}^{\beta}$  and local unit tangent to dislocation line  $\hat{\boldsymbol{t}}^{\beta}(\overline{\boldsymbol{x}})$ 

$$\overline{\overline{\alpha}}^{\beta}(\overline{x}) = \frac{1}{V_{sphere}} \int_{L} \overline{\overline{b}}^{\beta} \otimes \widehat{t}^{\beta}(\overline{x}) dL$$

Adapted from Arsenlis, Parks, Acta Mat. (1999)



## Theory of continuously represented dislocations: characterization



Adapted from Arsenlis, Parks, Acta Mat. (1999)

### A single dislocation on a slip system $\beta$

Characterized via Burgers vector  $\overline{\boldsymbol{b}}^{\rho}$  and local unit tangent to dislocation line  $\hat{\boldsymbol{t}}^{\beta}(\overline{\boldsymbol{x}})$ 

$$\overline{\overline{\boldsymbol{\alpha}}}^{\beta}(\overline{\boldsymbol{x}}) = \frac{1}{V_{sphere}} \int_{L} \overline{\boldsymbol{b}}^{\beta} \otimes \widehat{\boldsymbol{t}}^{\beta}(\overline{\boldsymbol{x}}) dL$$

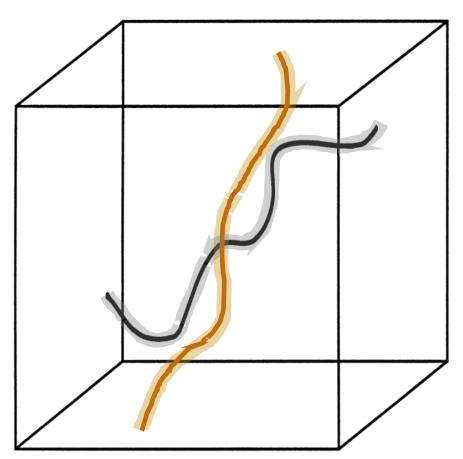
#### Multiple dislocations on different slip systems

$$\overline{\overline{\alpha}}(\overline{x}) = \sum_{\beta} \overline{\overline{\alpha}}^{\beta}(\overline{x}) = \frac{1}{V_{sphere}} \int_{L} \sum_{\beta} \overline{b}^{\beta}(\overline{x}) \otimes \hat{t}^{\beta}(\overline{x}) \, dL$$

Nye's polar dislocation density tensor (Nye 1953)

<u>Continuity condition</u>: div  $\overline{\overline{\alpha}} = 0$ 

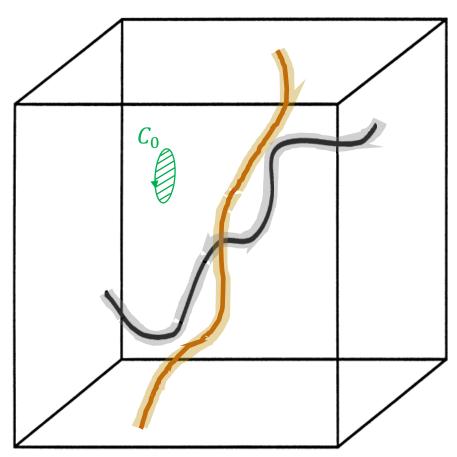




Assume simply connected domain Total displacement  $\overline{u}$  continuous everywhere =>  $[\![\overline{u}]\!] = 0$ Total distortion:  $\overline{\overline{U}}^{\parallel} = \operatorname{grad} \overline{u} = \nabla \overline{u}$  ("||" => <u>compatible</u>) curl  $\overline{\overline{U}}^{\parallel} = 0$ 

Adapted from Arsenlis, Parks, Acta Mat. (1999)



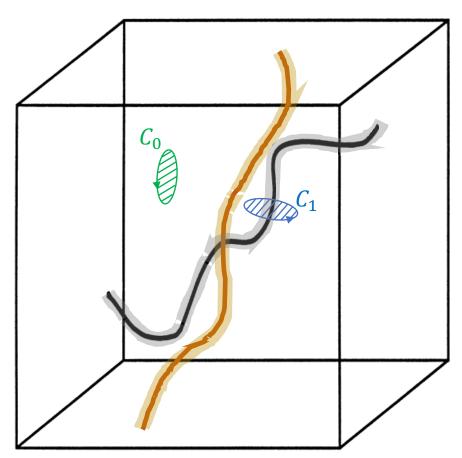


Assume simply connected domain Total displacement  $\overline{u}$  continuous everywhere =>  $[\![\overline{u}]\!] = 0$ Total distortion:  $\overline{\overline{U}}^{\parallel} = \operatorname{grad} \overline{u} = \nabla \overline{u}$  ("||" => compatible) curl  $\overline{\overline{U}}^{\parallel} = 0$ 

<u>Locations without dislocations</u> (Circuit  $C_0$ )  $\llbracket \overline{u}^e \rrbracket = \mathbf{0} \implies \overline{\overline{U}}^{e \parallel} = \mathbf{grad} \ \overline{u}^e \implies \mathbf{curl} \ \overline{\overline{U}}^{e \parallel} = \mathbf{0}$ 

Adapted from Arsenlis, Parks, Acta Mat. (1999)





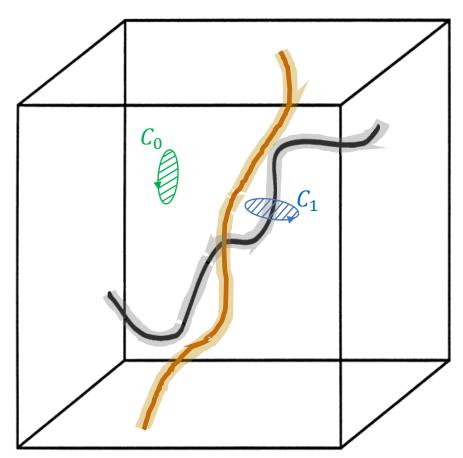
Adapted from Arsenlis, Parks, Acta Mat. (1999)



Assume simply connected domain Total displacement  $\overline{u}$  continuous everywhere =>  $[\![\overline{u}]\!] = 0$ Total distortion:  $\overline{\overline{U}}^{\parallel} = \operatorname{grad} \overline{u} = \nabla \overline{u}$  (" $\|$ " => compatible) curl  $\overline{\overline{U}}^{\parallel} = 0$ 

Locations without dislocations (Circuit  $C_0$ )  $\llbracket \overline{u}^e \rrbracket = \mathbf{0} \implies \overline{\overline{U}}^{e \parallel} = \operatorname{grad} \overline{u}^e \implies \operatorname{curl} \overline{\overline{U}}^{e \parallel} = \mathbf{0}$ 

<u>Locations with dislocations</u> (Circuit  $C_1$ )  $\overline{\boldsymbol{b}}^{\beta} = \left[\!\left[\overline{\boldsymbol{u}}^{e,\beta}\right]\!\right] = \int_{C_1} \overline{\overline{\boldsymbol{U}}}^{e,\beta} \cdot \overline{\boldsymbol{dL}} = \int_{S_1} \left(\operatorname{\mathbf{curl}} \overline{\overline{\boldsymbol{U}}}^{e,\beta}\right) \cdot \overline{\boldsymbol{n}}_1 \, dS \neq \mathbf{0}$ 



Adapted from Arsenlis, Parks, Acta Mat. (1999)

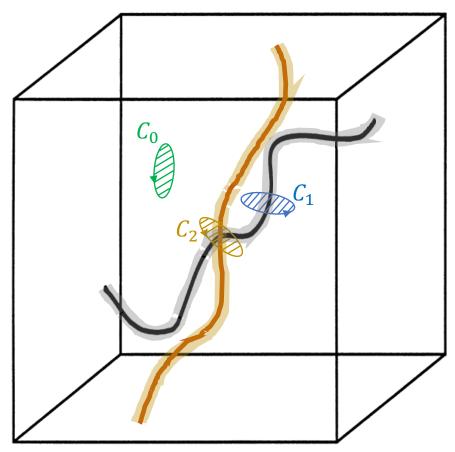
Assume simply connected domain Total displacement  $\overline{u}$  continuous everywhere =>  $[\![\overline{u}]\!] = 0$ Total distortion:  $\overline{\overline{U}}^{\parallel} = \operatorname{grad} \overline{u} = \nabla \overline{u}$  ("||" => compatible) curl  $\overline{\overline{U}}^{\parallel} = 0$ 

Locations without dislocations (Circuit  $C_0$ )  $\llbracket \overline{u}^e \rrbracket = \mathbf{0} \implies \overline{\overline{U}}^{e \parallel} = \operatorname{grad} \overline{u}^e \implies \operatorname{curl} \overline{\overline{U}}^{e \parallel} = \mathbf{0}$ 

cocations with dislocations (Circuit 
$$C_1$$
)  
$$\overline{\boldsymbol{b}}^{\beta} = \left[\!\left[\overline{\boldsymbol{u}}^{e,\beta}\right]\!\right] = \int_{C_1} \overline{\overline{\boldsymbol{U}}}^{e,\beta} \cdot \overline{\boldsymbol{dL}} = \int_{S_1} \left(\underbrace{\operatorname{curl}}_{\overline{\boldsymbol{u}}} \overline{\overline{\boldsymbol{u}}}^{e,\beta}\right) \cdot \overline{\boldsymbol{n}}_1 \, dS \neq \mathbf{0}$$
$$\overline{\overline{\boldsymbol{\alpha}}}^{\beta}$$

 $\operatorname{curl} \overline{\overline{U}}^{e,\beta} \neq \mathbf{0} \Rightarrow \ \overline{\overline{U}}^{e,\beta} \neq \overline{\overline{U}}^{e,\beta \parallel}$ 

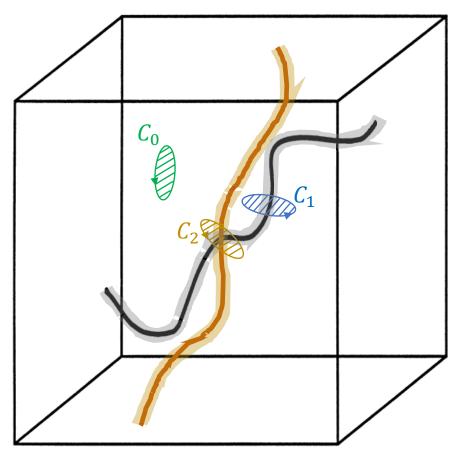




Locations with multiple dislocations (Circuit  $C_2$ )  $\overline{\boldsymbol{b}} = \left[\!\left[\overline{\boldsymbol{u}}^e\right]\!\right]^{\beta_1} + \left[\!\left[\overline{\boldsymbol{u}}^e\right]\!\right]^{\beta_2} = \int_{C_3} \overline{\overline{\boldsymbol{U}}}^e \cdot \overline{\boldsymbol{dL}} = \int_{S_3} \underbrace{\operatorname{curl}}_{\overline{\overline{\boldsymbol{u}}}} \overline{\overline{\boldsymbol{U}}}^e \cdot \overline{\boldsymbol{n}}_3 \, dS \neq 0$   $\overline{\overline{\boldsymbol{\alpha}}}$ 

Adapted from Arsenlis, Parks, Acta Mat. (1999)





Adapted from Arsenlis, Parks, Acta Mat. (1999)

Locations with multiple dislocations (Circuit  $C_2$ )  $\overline{\boldsymbol{b}} = \left[\!\left[\overline{\boldsymbol{u}}^e\right]\!\right]^{\beta_1} + \left[\!\left[\overline{\boldsymbol{u}}^e\right]\!\right]^{\beta_2} = \int_{C_3} \overline{\overline{\boldsymbol{U}}}^e \cdot \overline{\boldsymbol{dL}} = \int_{S_3} \underbrace{\operatorname{curl}}_{\overline{\overline{\boldsymbol{a}}}} \overline{\overline{\boldsymbol{U}}}^e \cdot \overline{\boldsymbol{n}}_3 \, dS \neq 0$   $\overline{\overline{\boldsymbol{a}}}$ 

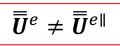
Now,

$$\overline{\overline{\alpha}} = \sum_{\beta} \overline{\overline{\alpha}}^{\beta} \Rightarrow \operatorname{curl} \overline{\overline{U}}^{e} = \sum_{\beta} \operatorname{curl} \overline{\overline{U}}^{e,\beta}$$

But

 $\overline{\overline{U}}^e \neq \sum_{\beta} \overline{\overline{U}}^{e^{\beta}}$ 

Also





### Stokes-Helmholtz type decomposition of $\overline{\overline{U}}^e$ Acharya and Roy JMPS 54 (2006) 1687 – 1710

Additive decomposition of  $\overline{m{U}}^e$  into compatible  $\overline{m{U}}^{e\parallel}$  and incompatible  $\overline{m{U}}^{e\perp}$ 

$$\overline{oldsymbol{U}}^e = \overline{oldsymbol{U}}^{e \parallel} + \overline{oldsymbol{U}}^{e \perp}$$
 in  $\Omega$ 



### Stokes-Helmholtz type decomposition of $\overline{\overline{U}}^e$ Acharya and Roy JMPS 54 (2006) 1687 – 1710

Additive decomposition of  $\overline{m{ar U}}^e$  into compatible  $\overline{m{ar U}}^{e\parallel}$  and incompatible  $\overline{m{ar U}}^{e\perp}$ 

$$\overline{\overline{U}}^e = \underbrace{\overline{\overline{U}}^{e\parallel}}_{\text{grad }\overline{w}} + \overline{\overline{U}}^{e\perp} \text{ in } \Omega$$

$$\operatorname{grad} \overline{w}, \text{ since } \operatorname{curl} \overline{\overline{U}}^{e\parallel} = \mathbf{0}$$



## Stokes-Helmholtz type decomposition of $\overline{m{ar{U}}}^e$

Acharya and Roy JMPS 54 (2006) 1687 – 1710

<u>Unique</u> additive decomposition of  $\overline{m{U}}^e$  into compatible  $\overline{m{U}}^{e\parallel}$  and incompatible  $\overline{m{U}}^{e\perp}$ 

$$\overline{\overline{U}}^{e} = \overline{\overline{U}}^{e\parallel} + \overline{\overline{U}}^{e\perp} \text{ in } \Omega$$

$$\mathbf{grad} \ \overline{w}, \text{ since } \mathbf{curl} \ \overline{\overline{U}}^{e\parallel} = \mathbf{0}$$

$$\mathbf{div} \ \overline{\overline{U}}^{e\perp} = \mathbf{0} \text{ in } \Omega$$

$$\overline{\overline{U}}^{e\perp} \cdot \overline{n} = \mathbf{0} \text{ on } \partial \Omega$$



## Stokes-Helmholtz type decomposition of $\overline{m{ar{U}}}^e$

Acharya and Roy JMPS 54 (2006) 1687 – 1710

<u>Unique</u> additive decomposition of  $\overline{m{U}}^e$  into compatible  $\overline{m{U}}^{e\parallel}$  and incompatible  $\overline{m{U}}^{e\perp}$ 

$$\overline{\overline{U}}^{e} = \overline{\overline{U}}^{e\parallel} + \overline{\overline{U}}^{e\perp} \text{ in } \Omega$$

$$\mathbf{grad} \ \overline{w}, \text{ since } \mathbf{curl} \ \overline{\overline{U}}^{e\parallel} = \mathbf{0}$$

$$\mathbf{div} \ \overline{\overline{U}}^{e\perp} = \mathbf{0} \text{ in } \Omega$$

$$\overline{\overline{U}}^{e\perp} \cdot \overline{n} = \mathbf{0} \text{ on } \partial \Omega$$

 $\Rightarrow \overline{\overline{\alpha}} = \operatorname{curl} \overline{\overline{U}}^e = \operatorname{curl} \overline{\overline{U}}^{e\perp} \neq \mathbf{0}$ 



### Elasto-static theory of dislocation fields

**Question**: Given  $\overline{\overline{\alpha}}^{\beta}$  (typically from experiments), how to obtain  $\overline{\overline{U}}^{e} = \overline{\overline{U}}^{e\parallel} + \overline{\overline{U}}^{e\perp}$ ?



## Elasto-static theory of dislocation fields

**Question**: Given  $\overline{\overline{\alpha}}^{\beta}$  (typically from experiments), how to obtain  $\overline{\overline{U}}^{e} = \overline{\overline{U}}^{e\parallel} + \overline{\overline{U}}^{e\perp}$ ?

Answer:

1) For  $\overline{\overline{U}}^{e\perp}$ : approach similar to the Helmholtz identity (curl curl  $\overline{\overline{\chi}} = \operatorname{grad} \operatorname{div} \overline{\overline{\chi}} - \Delta \overline{\overline{\chi}}$ )  $\overline{\overline{\alpha}} = \operatorname{curl} \overline{\overline{U}}^{e\perp}$  and  $\operatorname{div} \overline{\overline{U}}^{e\perp} = \mathbf{0}$  gives  $\Delta \overline{\overline{U}}^{e\perp} = -\operatorname{curl} \overline{\overline{\alpha}}$  (Acharya Roy JMPS 2006)



### Elasto-static theory of dislocation fields

**Question**: Given  $\overline{\overline{\alpha}}^{\beta}$  (typically from experiments), how to obtain  $\overline{\overline{U}}^{e} = \overline{\overline{U}}^{e\parallel} + \overline{\overline{U}}^{e\perp}$ ?

#### Answer:

1) For  $\overline{\overline{U}}^{e\perp}$ : approach similar to the Helmholtz identity (curl curl  $\overline{\overline{\chi}} = \operatorname{grad} \operatorname{div} \overline{\overline{\chi}} - \Delta \overline{\overline{\chi}}$ )  $\overline{\overline{\alpha}} = \operatorname{curl} \overline{\overline{U}}^{e\perp}$  and  $\operatorname{div} \overline{\overline{U}}^{e\perp} = \mathbf{0}$  gives  $\Delta \overline{\overline{U}}^{e\perp} = -\operatorname{curl} \overline{\overline{\alpha}}$  (Acharya Roy JMPS 2006)

2) For  $\overline{\overline{U}}^{e\parallel}$ : mechanical equilibrium and elastic law

Mechanical (static) equilibrium:  $\mathbf{div} \ \overline{\overline{\sigma}} = \mathbf{0}$ Elastic constitutive law:  $\overline{\overline{\sigma}} = \overline{\overline{\overline{c}}}$ :  $\overline{\overline{c}}^e = \overline{\overline{\overline{c}}}$ :  $\overline{\overline{U}}^e$ 

$$\sigma_{ij,j} = 0$$
  

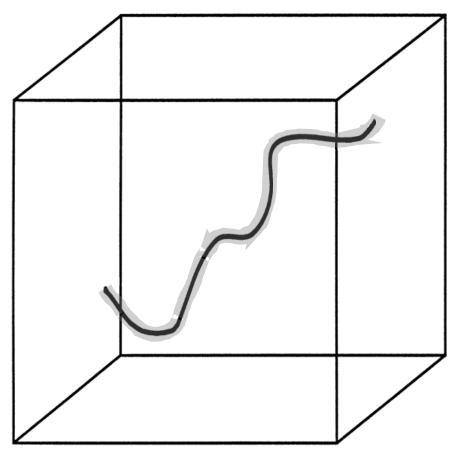
$$c_{ijkl}U_{kl,j}^{e\parallel} + f_i = 0$$
 with  $f_i = c_{ijkl}U_{kl,j}^{e\perp}$   

$$c_{ijkl}w_{k,lj} + f_i = 0$$
 with  $w_{k,l} = U_{kl}^{e\parallel}$ 

Solution using the Green's function approach!



### Plastic distortion field



Adapted from Arsenlis, Parks, Acta Mat. (1999)

Presence of a dislocation =>  $\overline{\overline{U}}^p \neq \mathbf{0}$ 

$$\begin{split} \overline{\overline{U}}^{\parallel} &= \overline{\overline{U}}^{e} + \overline{\overline{U}}^{p} = \overline{\overline{U}}^{e\parallel} + \overline{\overline{U}}^{e\perp} + \overline{\overline{U}}^{p\parallel} + \overline{\overline{U}}^{p\perp} \\ \Rightarrow \overline{\overline{U}}^{p\perp} &= -\overline{\overline{U}}^{e\perp} \end{split}$$

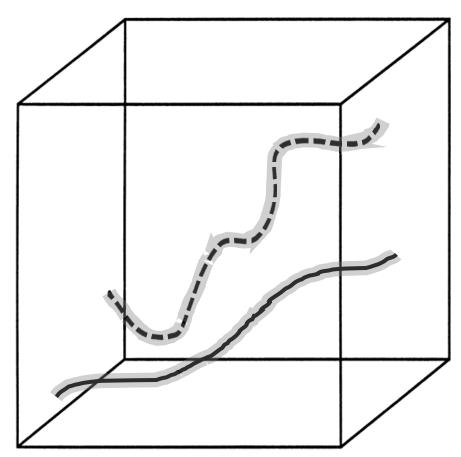
$$\begin{array}{l} \operatorname{curl} \overline{\overline{U}}^{e\perp} = \overline{\overline{\alpha}} = -\operatorname{curl} \overline{\overline{U}}^{p\perp} \\ \operatorname{div} \overline{\overline{U}}^{e\perp} = \mathbf{0} = \operatorname{div} \overline{\overline{U}}^{p\perp} \\ \overline{\overline{U}}^{e\perp} \cdot \overline{n} = \mathbf{0} = \overline{\overline{U}}^{p\perp} \cdot \overline{n} \end{array} \right] \quad \text{In } V \\ \end{array}$$

Given  $\overline{\overline{\pmb{\alpha}}}$ ,  $\overline{\overline{\pmb{U}}}^{p\perp}$  obtained using same procedure as  $\overline{\overline{\pmb{U}}}^{e\perp}$ 

Stationary case (no knowledge of history of dislocation motion) => Assume  $\overline{\overline{U}}^{p\parallel} = \mathbf{0}$ 



### Kinematics – transport of a single dislocation



Adapted from Arsenlis, Parks, Acta Mat. (1999)

Conservation of Burgers vector gives

$$\dot{\overline{b}}^{\beta} = \frac{\mathrm{d}}{\mathrm{d}t} \int_{S} \overline{\overline{a}}^{\beta} \cdot \overline{n} \, dS = \int_{S} \operatorname{curl} \overline{\overline{f}}^{\beta} \cdot \overline{n} \, dS + \int_{S} \overline{\overline{s}}^{\beta} \cdot \overline{n} \, dS$$
Flux
Source

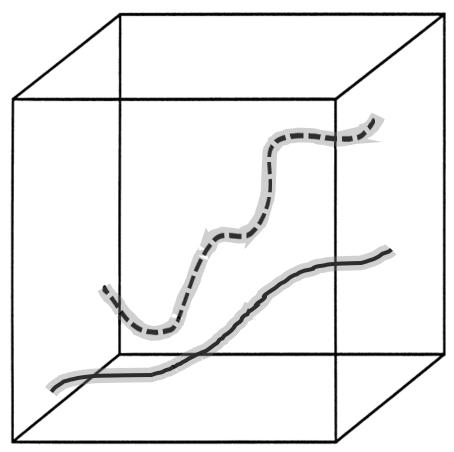
We can prove that  $\overline{\overline{f}}^{\beta} = -\overline{\overline{\alpha}}^{\beta} \times \overline{V}^{\beta} \rightarrow \text{Dislocation velocity}$ 

Local form:  $\dot{\overline{\alpha}}^{\beta} = -\operatorname{curl}\left(\overline{\overline{\alpha}}^{\beta} \times \overline{V}^{\beta}\right) + \overline{\overline{s}}^{\beta} - (\operatorname{Acharya} 2001)$ 

**Question:** How to obtain  $\overline{V}^{\beta}$ ?



### Dislocation velocity – 2<sup>nd</sup> law of thermodynamics



Adapted from Arsenlis, Parks, Acta Mat. (1999)

Power dissipated (Acharya 2003)

$$D = \int_{V} \overline{\overline{\sigma}} : \dot{\overline{\overline{U}}}^{p} dV = \int_{V} \sum_{\beta} \overline{F}^{\beta} \cdot \overline{V}^{\beta} dV \ge 0$$

With  $\overline{F}^{eta}=\overline{m{\sigma}}\cdot\overline{m{b}}^{eta} imesar{m{l}}^{eta}$  (Peach-Koehler force)

Question: How to obtain  $\overline{V}^{\beta}$ ? Answer: In theory, all  $\overline{V}^{\beta}$  that satisfy  $\int_{V} \sum_{\beta} \overline{F}^{\beta} \cdot \overline{V}^{\beta} dV \ge 0$  are admissible.

Simplest expression: 
$$\overline{V}^{\beta} = \frac{1}{B^{\beta}}\overline{F}^{\beta}$$
 with  $B^{\beta} > 0$ 



## Isothermal and adiabatic Elasto-plastic dynamic theory of dislocation fields (Acharya 2003)

- Incompatible elastic distortion and plastic distortion

div  $\overline{\overline{\sigma}} = \rho \overline{\overline{u}}$  $\overline{\overline{\sigma}} = \overline{\overline{\overline{C}}}: (\overline{\overline{U}}^{\parallel} - \overline{\overline{U}}^{p\parallel} - \overline{\overline{U}}^{p\perp})$ 

- dynamic equilibrium and elastic constitutive law

$$\overline{\boldsymbol{u}} = \overline{\boldsymbol{u}}^d \qquad \text{On } S^d_{body}$$
$$\overline{\boldsymbol{t}} = \overline{\boldsymbol{\sigma}} \cdot \overline{\boldsymbol{n}} \qquad \text{On } S^t_{body}$$

- Dirichlet and Neumann boundary conditions

 $\overline{\overline{\alpha}}^{\beta} = -\operatorname{curl}\left(\overline{\overline{\alpha}}^{\beta} \times \overline{V}^{\beta}\right) + \overline{\overline{s}}^{\beta} \qquad -\operatorname{Dislocal}^{\alpha}$ 

$$\overline{\boldsymbol{V}}^{\beta} = \frac{1}{B^{\beta}} \overline{\boldsymbol{F}}^{\beta} = \frac{1}{B^{\beta}} \left( \overline{\boldsymbol{\sigma}} \cdot \overline{\boldsymbol{b}}^{\beta} \times \overline{\boldsymbol{l}}^{\beta} \right)$$

Dislocation transport

– Dislocation velocity

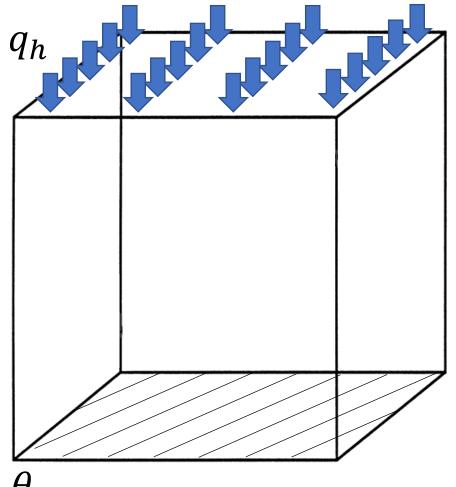
# The Thermal Field Dislocation Mechanics (T-FDM) model

Upadhyay, M. V., On the thermo-mechanical theory of field dislocations in transient heterogeneous temperature fields, *Journal of the Mechanics and Physics of Solids*, 105 (2020) 104150

### • Development

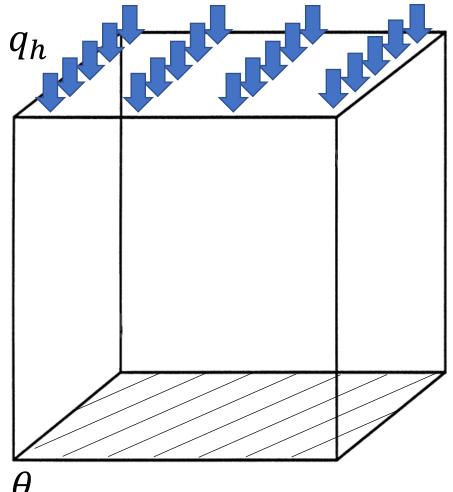
- The isothermal and adiabatic FDM model
- Heat conduction
- The new T-FDM model
- Model assumptions and impact on AM modelling





Boundary	Temperature	$\theta = \theta_a$	On $S^{ heta}_{body}$
<u>conditions</u>	Heat flux	$q_h = \overline{\boldsymbol{q}} \cdot \overline{\boldsymbol{n}}$	On $S^q_{body}$

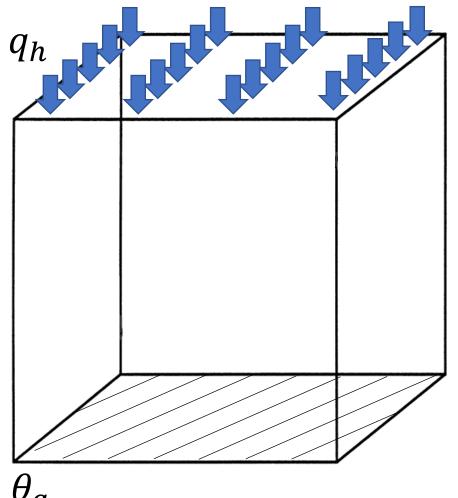
 $\theta_a$ 



Boundary	Temperature	$\theta = \theta_a$	On $S^{ heta}_{body}$		
conditions	Heat flux	$q_h = \overline{\boldsymbol{q}} \cdot \overline{\boldsymbol{n}}$	On S <sup>q</sup> <sub>body</sub>		
$   \underline{1^{st} law}:  \rho c_{v} \dot{\theta} = -\operatorname{div} \overline{\boldsymbol{q}} + \rho r \\   Internal energy \qquad \text{Heat loss} \\   change $					



https://www.manas-upadhyay.com

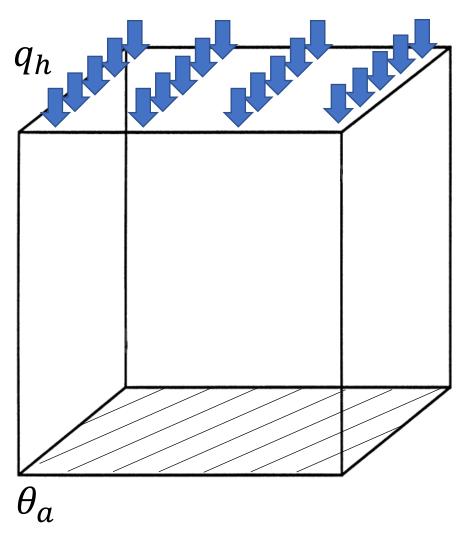


<u>Boundary</u> conditions	Temperature		On $S^{ heta}_{body}$		
	Heat flux	$q_h = \overline{\boldsymbol{q}} \cdot \overline{\boldsymbol{n}}$	On $S^q_{body}$		
$   \underline{1^{st}  \mathbf{law}}:  \underline{\rho c_{v} \dot{\theta}} = -\operatorname{div} \overline{\boldsymbol{q}} + \underline{\rho r} $ Internal energy Heat loss change					
and Lawy D					

**2nd law**: 
$$D = -\int_{V} \overline{\boldsymbol{q}} \cdot \overline{\boldsymbol{\nabla}\theta} \, dV \ge 0$$



https://www.manas-upadhyay.com



Boundary conditions	Temperature	$\theta = \theta_a$	On $S^{ heta}_{body}$			
	Heat flux	$q_h = \overline{\boldsymbol{q}} \cdot \overline{\boldsymbol{n}}$	On $S^q_{body}$			
$   \underline{1^{st}  \mathbf{law}}:  \underline{\rho c_{v} \dot{\theta}} = -\operatorname{div} \overline{\boldsymbol{q}} + \underline{\rho r} $ Internal energy Heat loss change						
$\underline{\mathbf{2^{nd}  law}}: \ D = -\int_{V} \overline{\boldsymbol{q}} \cdot \overline{\boldsymbol{\nabla}\theta} \ dV \ge 0$						
In theory, all $\overline{q}$ that satisfy $-\int_V \overline{q} \cdot \overline{\nabla \theta}  dV \ge 0$ are admissible.						
Simplest expression: $\overline{\boldsymbol{q}} = -\overline{\boldsymbol{k}} \cdot \overline{\boldsymbol{\nabla} \theta}$ with $\overline{\boldsymbol{k}}$ positive definite						
Fourier law of heat conduction						



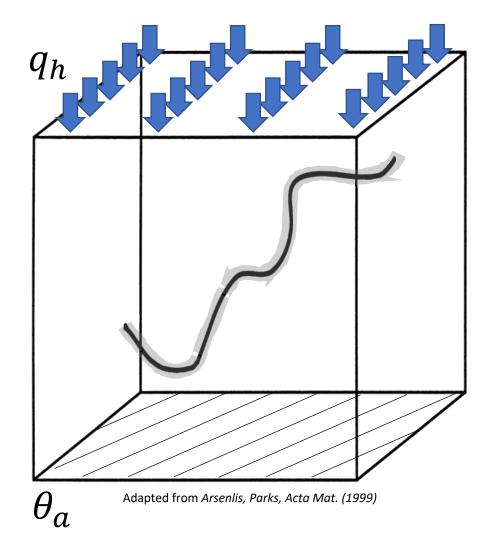
# The Thermal Field Dislocation Mechanics (T-FDM) model

Upadhyay, M. V., On the thermo-mechanical theory of field dislocations in transient heterogeneous temperature fields, *Journal of the Mechanics and Physics of Solids*, 105 (2020) 104150

### • Development

- The isothermal and adiabatic FDM model
- Heat conduction
- The new T-FDM model
- Model assumptions and impact on AM modelling

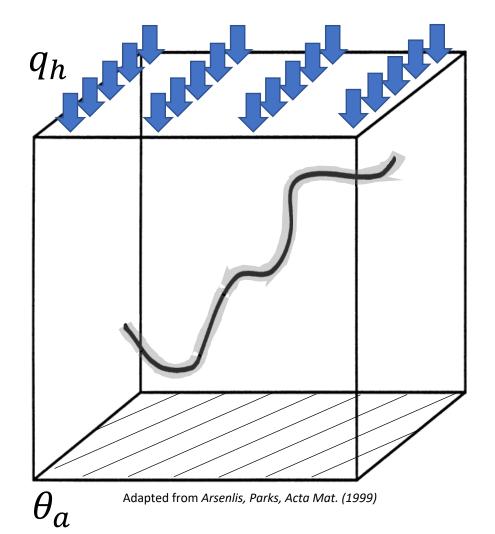




Presence of a heterogeneous temperature field

$$\overline{\overline{U}}^{\parallel} = \overline{\overline{U}}^{e} + \overline{\overline{U}}^{p} + \overline{\overline{\epsilon}}^{\theta} = \overline{\overline{U}}^{e\parallel} + \overline{\overline{U}}^{e\perp} + \overline{\overline{U}}^{p\parallel} + \overline{\overline{U}}^{p\perp} + ???$$





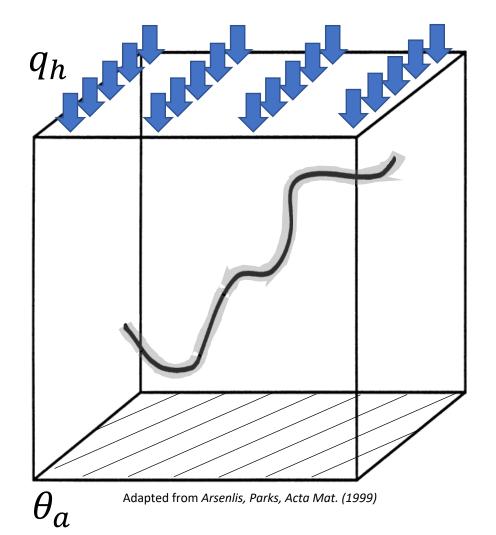
Presence of a heterogeneous temperature field

$$\overline{\overline{U}}^{\parallel} = \overline{\overline{U}}^{e} + \overline{\overline{U}}^{p} + \overline{\overline{\varepsilon}}^{\theta} = \overline{\overline{U}}^{e\parallel} + \overline{\overline{U}}^{e\perp} + \overline{\overline{U}}^{p\parallel} + \overline{\overline{U}}^{p\perp} + ???$$

Stokes-Helmholtz decomposition of  $\overline{\overline{\epsilon}}^{\theta}$ 

 $\overline{\overline{\boldsymbol{\varepsilon}}}^{\theta} = \overline{\overline{\boldsymbol{U}}}^{\theta \parallel} + \overline{\overline{\boldsymbol{U}}}^{\theta \perp}$ 

 $\overline{\overline{U}}^{\theta \parallel}, \overline{\overline{U}}^{\theta \perp}$  can be asymmetric They must satisfy  $\overline{\overline{U}}^{\theta \parallel} + \overline{\overline{U}}^{\theta \perp} = (\overline{\overline{U}}^{\theta \parallel} + \overline{\overline{U}}^{\theta \perp})^{\mathrm{T}}$ 



Presence of a heterogeneous temperature field

$$\overline{\overline{U}}^{\parallel} = \overline{\overline{U}}^{e} + \overline{\overline{U}}^{p} + \overline{\overline{\varepsilon}}^{\theta} = \overline{\overline{U}}^{e\parallel} + \overline{\overline{U}}^{e\perp} + \overline{\overline{U}}^{p\parallel} + \overline{\overline{U}}^{p\perp} + ???$$

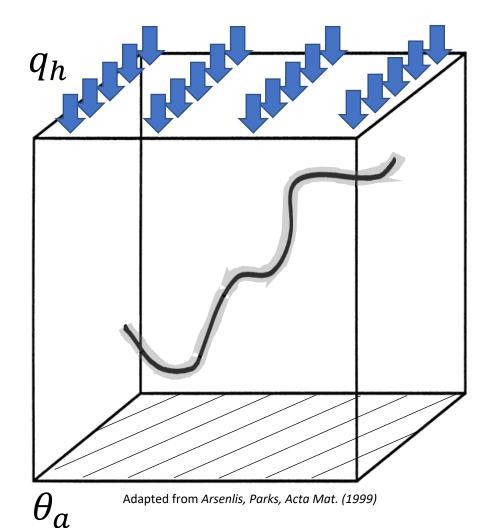
Stokes-Helmholtz decomposition of  $\overline{\overline{\epsilon}}^{\theta}$ 

 $\overline{\overline{\boldsymbol{\varepsilon}}}^{\boldsymbol{\theta}} = \overline{\overline{\boldsymbol{U}}}^{\boldsymbol{\theta} \parallel} + \overline{\overline{\boldsymbol{U}}}^{\boldsymbol{\theta} \perp}$ 

 $\overline{\overline{U}}^{\theta \parallel}, \overline{\overline{U}}^{\theta \perp}$  can be asymmetric They must satisfy  $\overline{\overline{U}}^{\theta \parallel} + \overline{\overline{U}}^{\theta \perp} = \left(\overline{\overline{U}}^{\theta \parallel} + \overline{\overline{U}}^{\theta \perp}\right)^{\mathrm{T}}$ 

$$\overline{\overline{U}}^{e\perp} = -\overline{\overline{U}}^{p\perp} - \overline{\overline{U}}^{\theta\perp}$$

Incompatible plastic and thermal distortions contribute to incompatible elastic distortion



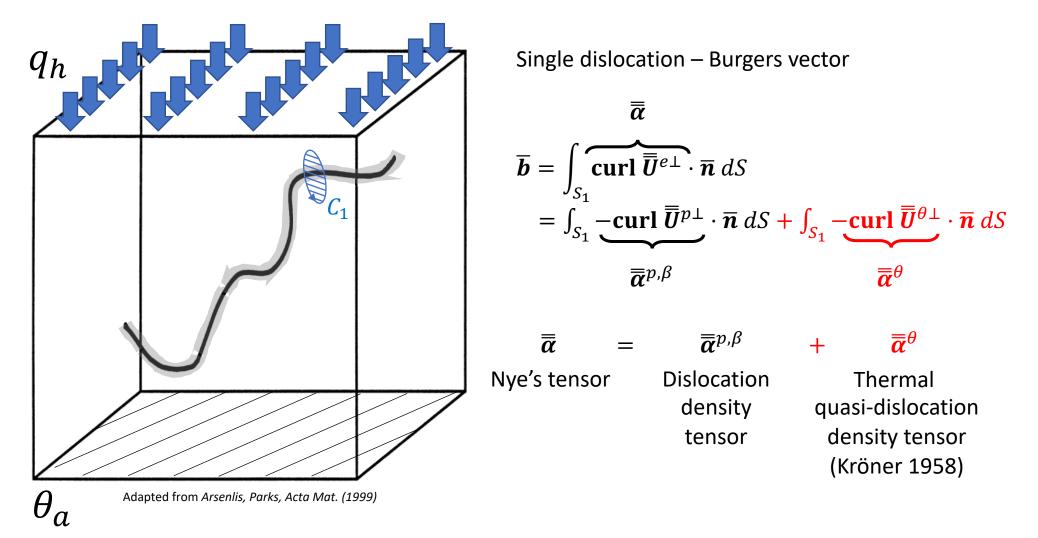
For applications, use empirical formula

$$\overline{\overline{\boldsymbol{\varepsilon}}}^{\theta} = \overline{\overline{\boldsymbol{\gamma}}}(\theta - \theta_0)$$

So what is the point of  $\overline{\overline{\epsilon}}^{\theta} = \overline{\overline{U}}^{\theta \parallel} + \overline{\overline{U}}^{\theta \perp}$ ?

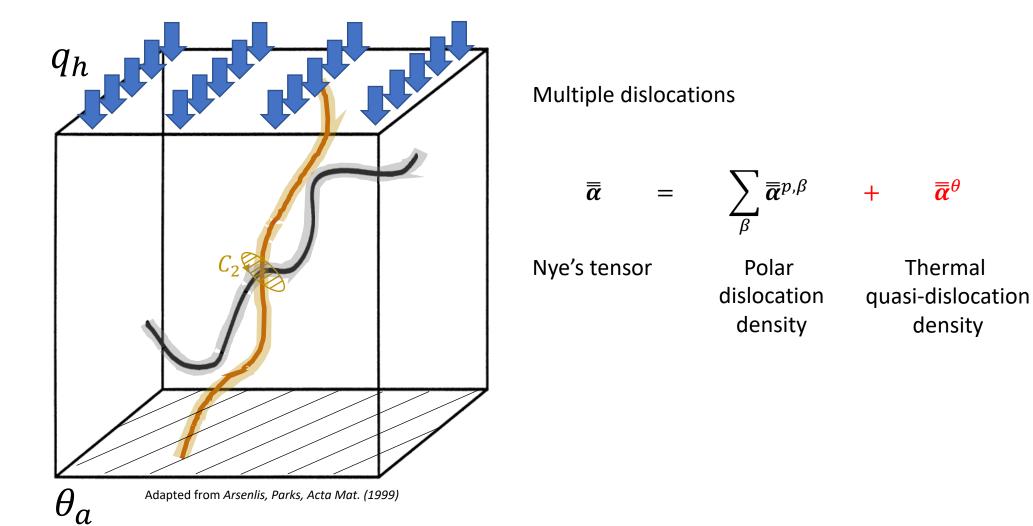
- Volumetric condition:  $\mathbf{div} \ \overline{\overline{U}}^{\theta \perp} = \mathbf{0}$ - Boundary condition:  $\overline{\overline{U}}^{\theta \perp} \cdot \overline{n} = \mathbf{0}$ 

# Theory of dislocation fields in a steady-state heterogeneous temperature field: Defect character





Theory of dislocation fields in a steady-state heterogeneous temperature field: Defect character

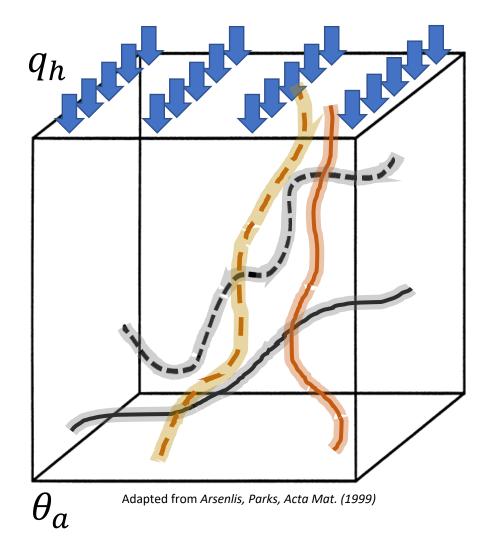




 $\overline{\overline{\alpha}}^{\theta}$ 

density

## Kinematics of dislocations in transient heterogeneous temperature fields



$$\frac{polar dislocation density}{\overline{\overline{\alpha}}^{p,\beta} = \operatorname{curl}\left(\overline{\overline{\alpha}}^{p,\beta} \times \overline{\overline{V}}^{\beta}\right) + \overline{\overline{S}}^{p,\beta}$$

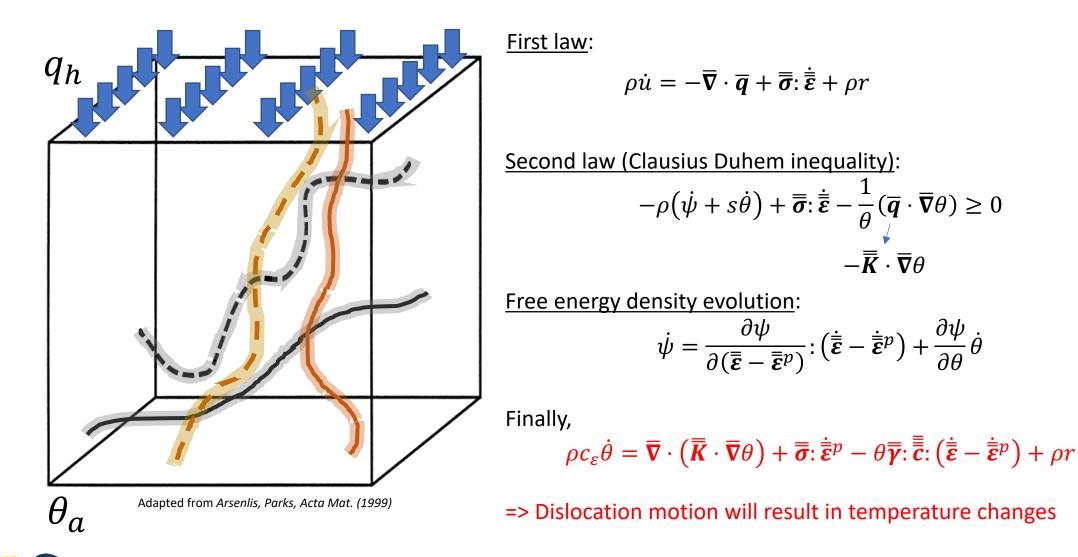
<u>Thermal quasi-dislocations</u>:  $\overline{\overline{\alpha}}^{\theta} = \nabla \times \overline{\overline{\overline{\epsilon}}}^{\theta} \approx -\overline{\overline{\gamma}} \cdot \left[ \nabla \overline{\theta} \cdot \overline{\overline{\overline{X}}} \right] \qquad 3^{rd} \text{ order Levi-Civita}$ permutation tensor

Nye's tensor:

$$\dot{\overline{\alpha}} = \operatorname{curl} \dot{\overline{\overline{U}}}^{e\perp} = \sum_{\beta} \left( \operatorname{curl} \left( \overline{\overline{\alpha}}^{p,\beta} \times \overline{\overline{V}}^{\beta} \right) + \overline{\overline{S}}^{p,\beta} \right) + \dot{\overline{\overline{\alpha}}}^{\theta}$$

- Absence of dislocations => Temperature changes result in evolution of  $\overline{\overline{\alpha}}$  and  $\overline{\overline{U}}^{e\perp}$
- Presence of dislocations
  - Temperature changes can be accommodated by dislocation density evolution without change to  $\overline{\overline{\alpha}}$  and  $\overline{\overline{U}}^{e\perp}$ 
    - => dislocation structures could form during rapid cooling without change to stress fields

Thermo-mechanical aspects of dislocation fields in transient temperature changes: Temperature evolution



# Dynamics of dislocation fields in transient heterogeneous temperature fields

 $\begin{array}{c} \mathbf{curl} \ \overline{\overline{U}}^{e\perp} = \overline{\overline{\alpha}} = -\mathbf{curl} \ \overline{\overline{U}}^{p\perp} - \mathbf{curl} \ \overline{\overline{U}}^{\theta\perp} \\ \mathbf{div} \ \overline{\overline{U}}^{e\perp} = \mathbf{div} \ \overline{\overline{U}}^{p\perp} = \mathbf{div} \ \overline{\overline{U}}^{\theta\perp} = \mathbf{0} \\ \overline{\overline{U}}^{e\perp} \cdot \overline{n} = \overline{\overline{U}}^{p\perp} \cdot \overline{n} = \overline{\overline{U}}^{\theta\perp} \cdot \overline{n} = \mathbf{0} \\ \end{array} \right] \quad \text{In } V$ 

– Incompatible elastic distortion and plastic distortion

div  $\overline{\overline{\sigma}} = \rho \overline{\overline{u}}$  $\overline{\overline{\sigma}} = \overline{\overline{\overline{c}}}: (\overline{\overline{U}} - \overline{\overline{U}}^{p\parallel} - \overline{\overline{U}}^{p\perp}) - \overline{\overline{\overline{c}}}: \overline{\overline{\gamma}}(\theta - \theta_0)$ 

- dynamic equilibrium and elastic constitutive law

 $\overline{\boldsymbol{u}} = \overline{\boldsymbol{u}}^{d} \quad \text{On } S^{d}_{body} \quad \theta = \hat{\theta} \quad \text{On } S^{\theta}_{body}$  $\overline{\boldsymbol{t}} = \overline{\boldsymbol{\sigma}} \cdot \overline{\boldsymbol{n}} \quad \text{On } S^{t}_{body} \quad q = \overline{\boldsymbol{q}}^{h} \cdot \overline{\boldsymbol{n}} \quad \text{On } S^{q}_{body}$ 

$$\frac{\overline{\overline{\alpha}}}{\overline{\overline{\alpha}}} = \sum_{\beta} \left[ -\operatorname{curl}\left(\overline{\overline{\alpha}}^{p,\beta} \times \overline{\overline{\nu}}^{\beta}\right) + \overline{\overline{S}}^{p,\beta} \right] + \frac{\overline{\overline{\alpha}}}{\overline{\overline{\alpha}}}^{\theta}$$

$$\overline{\overline{V}}^{\beta} = \frac{1}{B^{\beta}} \overline{\overline{F}}^{\beta} = \frac{1}{B^{\beta}} \left(\overline{\overline{\sigma}} \cdot \overline{\overline{b}}^{\beta} \times \overline{\overline{l}}^{\beta}\right)$$

https://www.manas-upadhyay.com

CNTS

Dirichlet and Neumann boundary conditions

- Dislocation and thermal-quasi dislocation evolution

- Dislocation velocity

Upadhyay, JMPS 105 (2020) 104150

 $\rho c_{\varepsilon} \dot{\theta} = \overline{\nabla} \cdot \left(\overline{\overline{K}} \cdot \overline{\nabla} \theta\right) + \overline{\overline{\sigma}} : \dot{\overline{\overline{\varepsilon}}}^p - \theta \overline{\overline{\gamma}} : \dot{\overline{\overline{\varepsilon}}} : \left(\dot{\overline{\overline{\varepsilon}}} - \dot{\overline{\overline{\varepsilon}}}^p\right) + \rho r - \text{Internal energy balance}$  $\overline{q} = -\overline{\overline{K}} \cdot \overline{\nabla} \theta \qquad \qquad - \text{Fourier law of heat conduction}$ 

# The Thermal Field Dislocation Mechanics (T-FDM) model

Upadhyay, M. V., On the thermo-mechanical theory of field dislocations in transient heterogeneous temperature fields, *Journal of the Mechanics and Physics of Solids*, 105 (2020) 104150

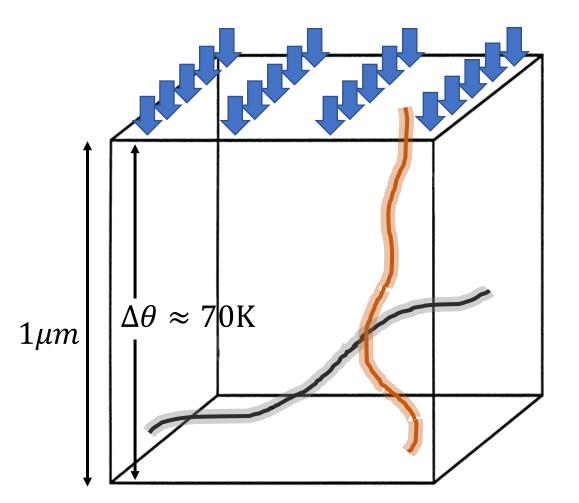
### • Development

- The isothermal and adiabatic FDM model
- Heat conduction
- The new T-FDM model

### Model assumptions and impact on AM modelling

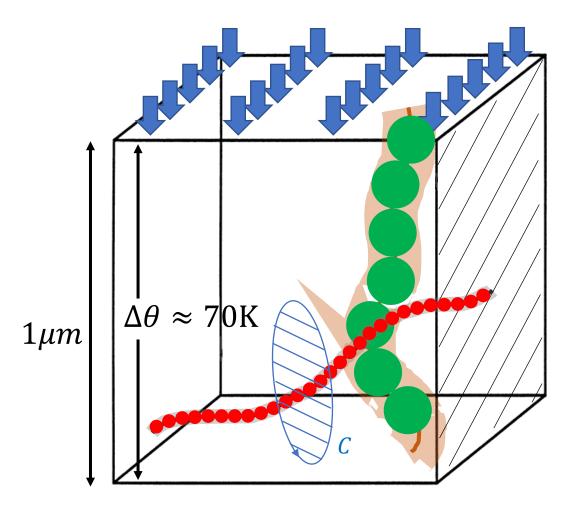


## Model assumptions and impact on AM modeling

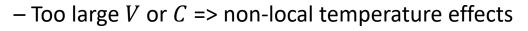


- Local thermodynamic equilibrium
  - Highest  $\dot{\theta}$  during SSTC  $\approx 10^6 \ K/s$
  - $-\ln 10^{-12}s$ ,  $\Delta\theta = 10^{-6}K$
  - Atomic fluctuations corresponding to thermal equilibrium for  $\Delta t > 10^{-12}s$
  - ⇒ Thermal equilibrium instantaneously achieved compared to changes in boundary condition
     Model is suitable to simulate DD during AM

## Model assumptions and impact on AM modeling



- Local thermodynamic equilibrium
  - Highest  $\dot{\theta}$  during SSTC  $\approx 10^6 \ K/s$
  - $-\ln 10^{-12}s$ ,  $\Delta\theta = 10^{-6}K$
  - Atomic fluctuations corresponding to thermal equilibrium for  $\Delta t > 10^{-12}s$
  - ⇒ Thermal equilibrium instantaneously achieved compared to changes in boundary condition
     Model is suitable to simulate DD during AM
- Need careful treatment during upscaling



## Summary

- The thermo-mechanically rigorous T-FDM model captures
  - Isothermal/adiabatic dislocation dynamics
    - +
  - Dislocation generation/annihilation/motion/density evolution due to temperature evolution
    - +
  - Temperature changes induced by moving dislocations

Upadhyay, M. V., On the thermo-mechanical theory of field dislocations in transient heterogeneous temperature fields, *Journal of the Mechanics and Physics of Solids*, 105 (2020) 104150.

https://doi.org/10.1016/j.jmps.2020.104150

